

# The Development of the Oloid

Hans Dirnböck\* and Hellmuth Stachel<sup>×</sup>

*\*Institute of Mathematics, University Klagenfurt  
Universitätsstr. 65, A-9020 Klagenfurt, Austria*

*<sup>×</sup>Institute of Geometry, Vienna University of Technology  
Wiedner Hauptstr. 8-10/113, A-1040 Wien, Austria  
email: stachel@geometrie.tuwien.ac.at*

**Abstract.** Let two unit circles  $k_A, k_B$  in perpendicular planes be given such that each circle contains the center of the other. Then the convex hull of these circles is called *Oloid*. In the following some geometric properties of the Oloid are treated analytically. It is proved that the development of the bounding torse  $\Psi$  leads to elementary functions only. Therefore it is possible to express the rolling of the Oloid on a fixed tangent plane  $\tau$  explicitly. Under this staggering motion, which is related to the well-known spatial Turbula-motion, also an ellipsoid  $\Phi$  of revolution inscribed in the Oloid is rolling on  $\tau$ . We give parameter equations of the curve of contact in  $\tau$  as well as of its counterpart on  $\Phi$ .

The surface area of the Oloid is proved to equal the area of the unit sphere. Also the volume of the Oloid is computed.

*Keywords:* Oloid, Turbula-motion, development of torsos.

*MSC 1994:* 51N05, 53A05, 53A17

## 1 Introduction

Let  $k_A, k_B$  be two unit circles in perpendicular planes  $\Pi_1, \Pi_2$  such that  $k_A$  passes through the center  $M_B$  of  $k_B$  and  $k_B$  passes through the center  $M_A$  of  $k_A$  (see Fig. 1)<sup>1</sup>. The *torse* (developable)  $\Psi$  connecting  $k_A$  and  $k_B$  is the enveloping surface of all planes  $\tau$  that touch  $k_A$  and  $k_B$  simultaneously. If any tangent plane  $\tau$  contacts  $k_A$  at  $A$  and  $k_B$  at  $B$ , then the line  $AB$  is a generator of  $\Psi$ . In this case the tangent line of  $k_A$  at  $A$  must intersect the tangent line of  $k_B$  at  $B$  in a finite or infinite point  $T$  on the line  $l_2$  of intersection between  $\Pi_1$  and  $\Pi_2$  (see Fig. 2; the triangle  $ABT$  can also be found in Fig. 5 and Fig. 6).

---

<sup>1</sup>All figures in this paper are orthogonal views. But only in Fig. 5 and Fig. 6 the superscript “ $n$ ” is used to indicate that geometric objects have been projected orthogonally into a plane.

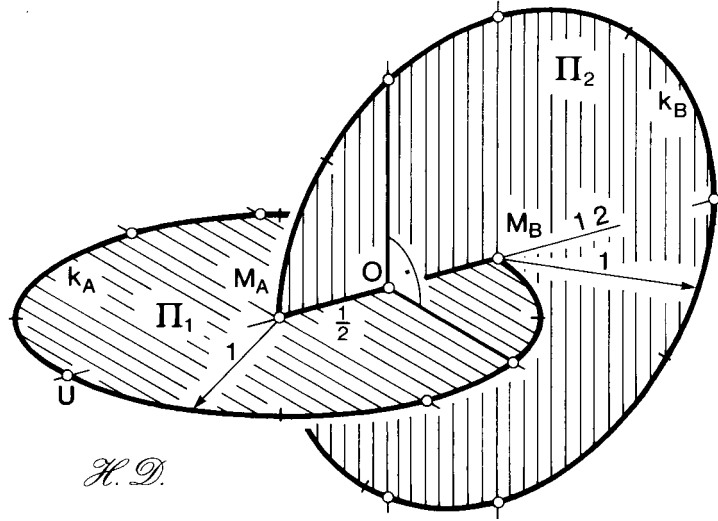


Figure 1: Circles  $k_A, k_B$  defining the Oloid

We choose the planes  $\Pi_1, \Pi_2$  as coordinate planes and the midpoint  $O$  of  $M_A M_B$  as the origin of a cartesian coordinate system. Then we may set up the equations of  $k_A, k_B$  as

$$(1) \quad \begin{aligned} k_A: x^2 + (y + \frac{1}{2})^2 &= 1 & \text{and} & \quad z = 0 \\ k_B: (y - \frac{1}{2})^2 + z^2 &= 1 & \text{and} & \quad x = 0. \end{aligned}$$

We parametrize the torse  $\Psi$  by the arc-length  $t$  of  $k_A$  with the starting point  $t = 0$  at  $U$  on

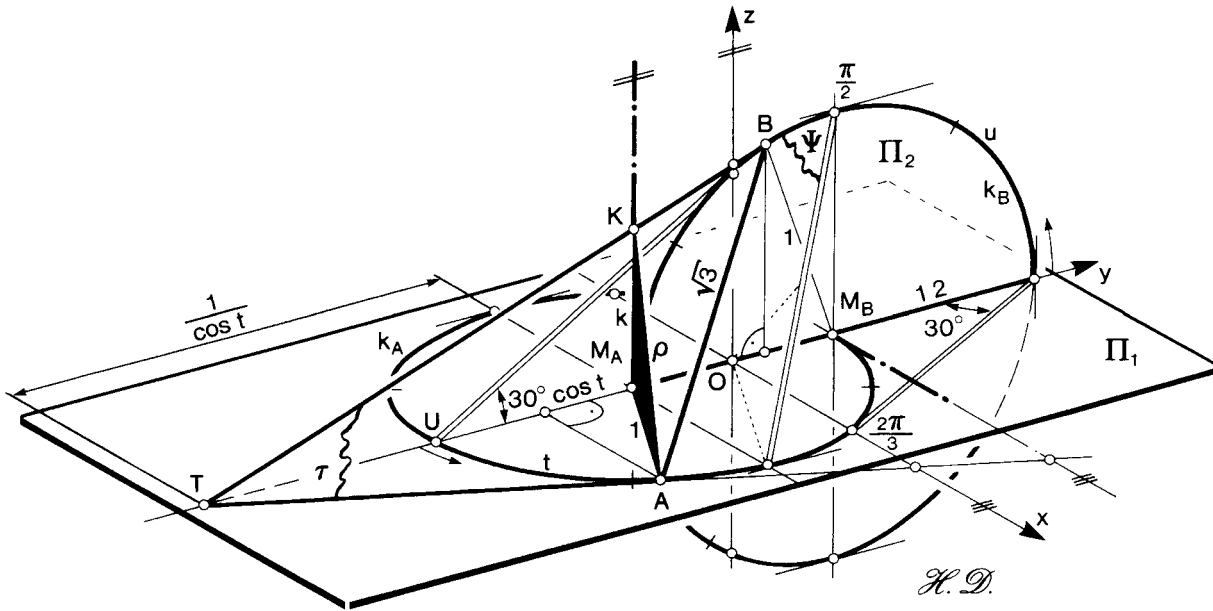


Figure 2: Coordinate system and notation

the negative  $y$ -axis. Then we obtain the coordinates

$$(2) \quad A = \left( \sin t, -\frac{1}{2} - \cos t, 0 \right).$$

Since the point  $T$  on the  $y$ -axis is conjugate to  $A$  with respect to  $k_A$ , we get

$$(3) \quad T = \left( 0, -\frac{2 + \cos t}{2 \cos t}, 0 \right).$$

In the same way conjugacy between  $T$  and  $B$  with respect to  $k_B$  implies

$$(4) \quad B = \left( 0, \frac{1}{2} - \frac{\cos t}{1 + \cos t}, \pm \frac{\sqrt{1 + 2 \cos t}}{1 + \cos t} \right).$$

The upper sign of the  $z$ -coordinate corresponds to the upper half of  $\Psi$ .<sup>2</sup>

From (2) and (4) we compute the squared length of the line segment  $AB$  as

$$\overline{AB}^2 = \sin^2 t + \left( 1 + \cos t - \frac{\cos t}{1 + \cos t} \right)^2 + \frac{1 + 2 \cos t}{(1 + \cos t)^2} = \sin^2 t + (1 + \cos t)^2 - 2 \cos t + 1,$$

which results in

**Theorem 1:** *All line segments  $AB$  of the torse  $\Psi$  are of equal length*

$$(5) \quad \overline{AB} = \sqrt{3}.$$

*This surprising result has already been proved in [7]. But probably also P. SCHATZ was aware of this result when he took out a patent for the Oloid (cf. [8]) in 1933 (see also [9], Figures 155, 156 and p. 122).*

Let  $u$  denote the arc-length of  $k_B$ , starting on the positive  $y$ -axis. Then  $A \in k_A$  and  $B \in k_B$  are points of the same generator of  $\Psi$  if and only if the parameters  $t$  of  $A$  and  $u$  of  $B$  obey the involutive relation

$$(6) \quad \cos u = -\frac{\cos t}{1 + \cos t} \quad \text{or} \quad \cos^2 \frac{t}{2} \cos^2 \frac{u}{2} = \frac{1}{4}.$$

For real generators of  $\Psi$  the condition  $1 + 2 \cos t \geq 0$  is necessary. By the restriction

$$(7) \quad -\frac{2\pi}{3} < t < \frac{2\pi}{3} \quad \text{and} \quad -\frac{2\pi}{3} < u < \frac{2\pi}{3}$$

we avoid vanishing denominators. It has to be noted that for  $\Psi$  the parametrization by  $t$  becomes singular at  $t = \pm 2\pi/3$ .

In the following we restrict each generator of  $\Psi$  to the line segment  $AB$ . Thus we obtain just the boundary of the *convex hull* of  $k_A$  and  $k_B$ .

## 2 Development of the Torse $\Psi$

When  $\Psi$  is developed into a plane  $\tau$ , then the circles  $k_A, k_B$  are isometrically transformed into planar curves  $k_A^d, k_B^d$ , respectively. It is well-known from Differential Geometry (see e.g. [11], p. 209 or [12], p. 72) that at corresponding points  $A \in k_A \subset \Psi$  and  $A^d \in k_A^d \subset \tau$  the geodesic curvatures are equal. This can be expressed in a more geometric way as follows (cf. [4], p. 295): When  $\tau$  is specified as the tangent plane of  $\Psi$  along the generator  $AB$ , then the curvature

---

<sup>2</sup>In the generalization presented in [5] the circles  $k_A, k_B$  are replaced by congruent ellipses with a common axis.

center  $K$  of  $k_A^d$  at  $A^d = A$  is located on the curvature axis of  $k_A$  at  $A$ , which is the axis of revolution of (the curvature circle)  $k_A$  (see Fig. 2, compare Fig. 3). Since  $K = (-\frac{1}{2}, 0, \pm k)^3$  is aligned with  $T$  and  $B$ , we get for the squared curvature radius

$$\rho^2 = \overline{AK}^2 = 1 + k^2 = \frac{2 + 2 \cos t}{1 + 2 \cos t}.$$

Hence the curvature  $\kappa$  of  $k_A^d$  reads

$$(8) \quad \frac{1}{\rho} = \kappa(t) = \sqrt{\frac{1 + 2 \cos t}{2(1 + \cos t)}}.$$

This is the so-called natural equation of  $k_A^d$  with arc-length  $t$ .<sup>4</sup>

In order to deduce an explicit representation of  $k_A^d$ , we choose  $\tau$  as the tangent plane at the point  $U \in k_A$  with minimal  $y$ -coordinate. In  $\tau$  we introduce a cartesian coordinate system with origin  $U^d = U$  and axes  $I$  and  $II$  (see Fig. 3). We define the first coordinate-axis  $I$  parallel to the tangent vector of  $k_A$  at  $U$ . Then due to RICCATI's formula (see e.g. [10], p. 44) we get

$$(9) \quad \begin{aligned} I_A(t) &= I_0 + \int_0^t \cos \alpha(t) dt \\ II_A(t) &= II_0 + \int_0^t \sin \alpha(t) dt \end{aligned} \quad \text{for } \alpha(t) := \alpha_0 + \int_0^t \kappa(t) dt$$

with the specifications  $\alpha_0 = I_0 = II_0 = 0$ . By integration of (8) we obtain

$$(10) \quad \alpha(t) = 2 \arcsin \frac{\sqrt{6} \sin t}{3\sqrt{1 + \cos t}} - \arcsin \frac{\sqrt{3} \tan \frac{t}{2}}{3}.$$

**Theorem 2:** *In the cartesian coordinate system  $(I, II)$  (see Fig. 4) the arc length parametrization of the development  $k_A^d$  of the circle  $k_A$  reads*

$$(11) \quad \begin{aligned} I_A(t) &= \frac{2\sqrt{3}}{9} \left[ \sqrt{2(1 + 2 \cos t)(1 - \cos t)} + \arccos \frac{\sqrt{2} \cos t}{\sqrt{1 + \cos t}} \right] \\ II_A(t) &= \frac{\sqrt{3}}{9} \left[ 4(1 - \cos t) + \ln \frac{2}{1 + \cos t} \right]. \end{aligned}$$

*Proof:* The integrals in the left column of (9) could not be immediately solved with the use of common computer-algebra-systems. We succeeded as follows: The integral for  $II_A(t)$  can be transformed into

$$\begin{aligned} II_A(t) &= \int_0^t \sin \left( 2 \arcsin \frac{\sqrt{6} \sin t}{3\sqrt{1 + \cos t}} - \arcsin \frac{\sqrt{3} \tan \frac{t}{2}}{3} \right) dt = \\ &= \int_0^t \left[ \frac{4\sqrt{6} \sin \frac{t}{2} (1 + 2 \cos t)}{9 \sqrt{1 + \cos t}} - \frac{\sqrt{3} \tan \frac{t}{2} (4 \cos t - 1)}{9} \right] dt, \end{aligned}$$

and this gives rise to the second equation in (11). From

$$(12) \quad \frac{dII_A}{dt} = \frac{\sqrt{3}}{9} \sin t \left( 4 + \frac{1}{1 + \cos t} \right) = \sin \alpha$$

<sup>3</sup>The sign of the  $z$ -coordinate is equal to that of  $B$  in (4).

<sup>4</sup>Note  $\dot{\rho}(0) = 0$ , but  $\ddot{\rho}(0) = \frac{1}{18}\sqrt{3} \neq 0$ . This proves that at  $U^d$  there is exactly a four-point contact between  $k_A^d$  and its curvature circle (see Fig. 4 or Fig. 5).



due to (9) we obtain

$$(13) \quad \frac{dI_A}{dt} = \cos \alpha = \sqrt{1 - \left(\frac{dII_A}{dt}\right)^2} = \frac{\sqrt{6}(1 + 2 \cos t)^{\frac{3}{2}}}{9\sqrt{1 + \cos t}}.$$

Then the integration can be carried out using the substitution  $\bar{t} := \tan \frac{t}{2}$ . The first quarter of the developed curve  $k_A^d$  ends at

$$\left(I_A\left(\frac{2\pi}{3}\right), II_A\left(\frac{2\pi}{3}\right)\right) = \left(\frac{2\pi\sqrt{3}}{9}, \frac{2\sqrt{3}}{9}(3 + \ln 2)\right) \approx (1.2092, 1.4215). \quad \square$$

There is an analogous representation of the developed image  $k_B^d$  of the circle  $k_B$  in terms of its arc-length  $u$ . The curves  $k_A^d$  and  $k_B^d$  are congruent since halfturns about the axes  $x \pm z = y = 0$  interchange  $k_A$  and  $k_B$  while the Oloid is transformed into itself. However, based on (11) and due to (5) the curve  $k_B^d$  can also be parametrized in the form

$$(14) \quad \begin{aligned} I_B(t) &= I_A(t) + \sqrt{3} \cos \epsilon_{AB}, \\ II_B(t) &= II_A(t) + \sqrt{3} \sin \epsilon_{AB}. \end{aligned}$$

Here the angle  $\epsilon_{AB} = \alpha + \gamma$  (see Fig. 4) defines the direction of the developed generator  $A^d B^d$ . Angle  $\alpha$  has already been computed in (12) and (13).  $\gamma$  is the angle made by the generator  $AB$  of  $\Psi$  and the tangent vector

$$(15) \quad \mathbf{v}_A = (\cos t, \sin t, 0)$$

of  $k_A$  at  $A$ . The dot product of  $\mathbf{v}_A$  and the vector  $\overrightarrow{AB}$  according to (2) and (4) gives

$$\sqrt{3} \cos \gamma = \mathbf{v}_A \cdot \overrightarrow{AB} = -\sin t \cos t + \sin t + \sin t \cos t - \frac{\sin t \cos t}{1 + \cos t} = \frac{\sin t}{1 + \cos t}.$$

Elementary trigonometry leads to

$$(16) \quad \sin \gamma = \sqrt{\frac{2(1 + 2 \cos t)}{3(1 + \cos t)}}$$

and finally to

$$(17) \quad \begin{aligned} \sin \epsilon_{AB} &= \frac{7 + 7 \cos t + 4 \cos^2 t}{9(1 + \cos t)} \\ \cos \epsilon_{AB} &= -\frac{2\sqrt{2}(2 + \cos t)\sqrt{(1 - \cos t)(1 + 2 \cos t)}}{9(1 + \cos t)}. \end{aligned}$$

We substitute these formulas in (14). Then due to (11) we obtain

**Theorem 3:** *In the cartesian coordinate system  $(I, II)$  of  $\tau$  (see Fig. 4 or Fig. 3) the development  $k_B^d$  of the circle  $k_B$  has the parametrization with respect to the arc-length  $t$  of  $k_A$  as follows:*

$$(18) \quad \begin{aligned} I_B(t) &= \frac{2\sqrt{3}}{9} \left[ \arccos \frac{\sqrt{2} \cos t}{\sqrt{1 + \cos t}} - \frac{\sqrt{2(1 - \cos t)(1 + 2 \cos t)}}{(1 + \cos t)} \right] \\ II_B(t) &= \frac{\sqrt{3}}{9} \left[ \ln \frac{2}{1 + \cos t} + \frac{11 + 7 \cos t}{1 + \cos t} \right]. \end{aligned}$$

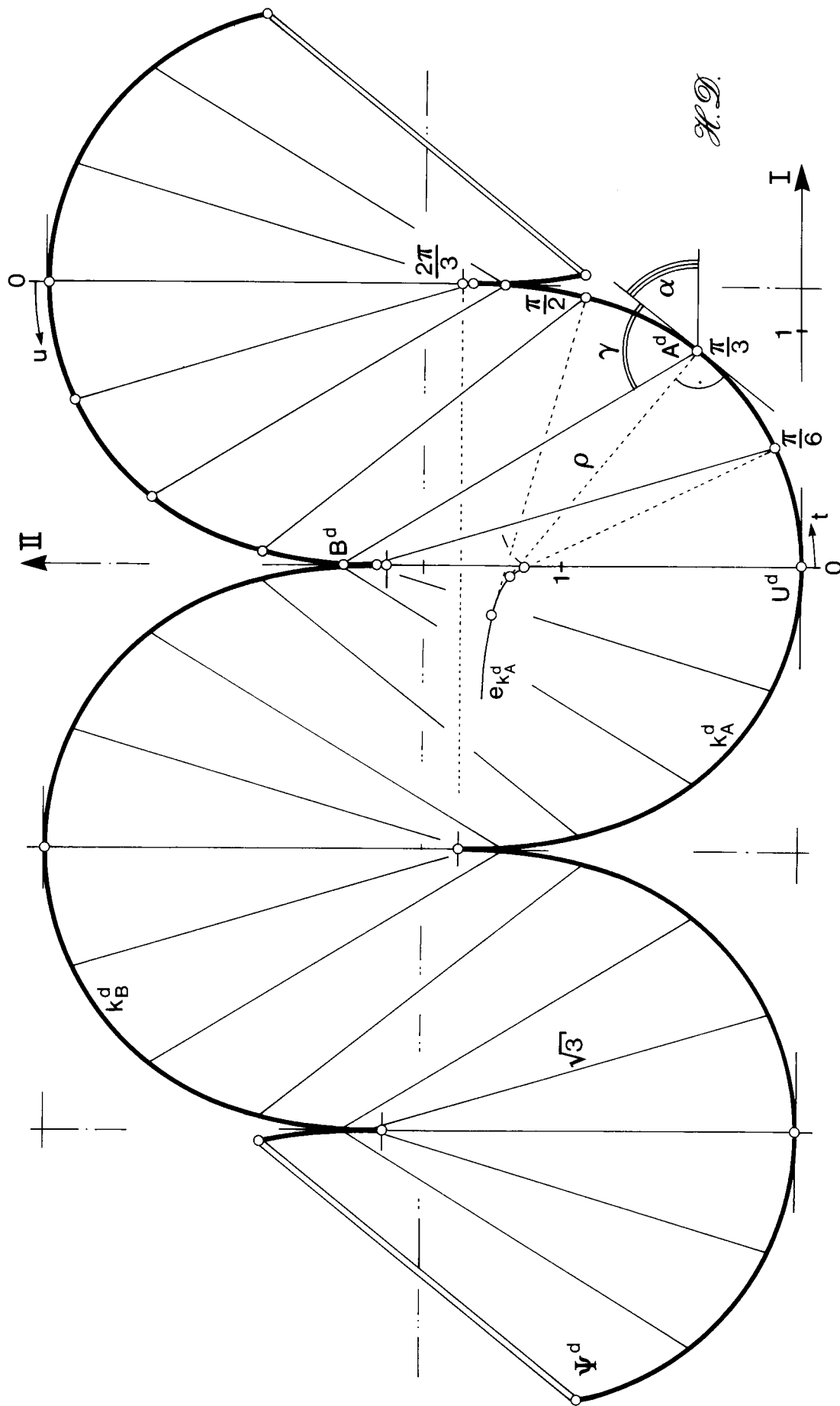


Figure 4: The development of the Oloid with the images  $k_A^d$  of  $k_A$  and  $k_B^d$  of  $k_B$  together with the evolute  $e_{k_A^d}$  of  $k_A^d$

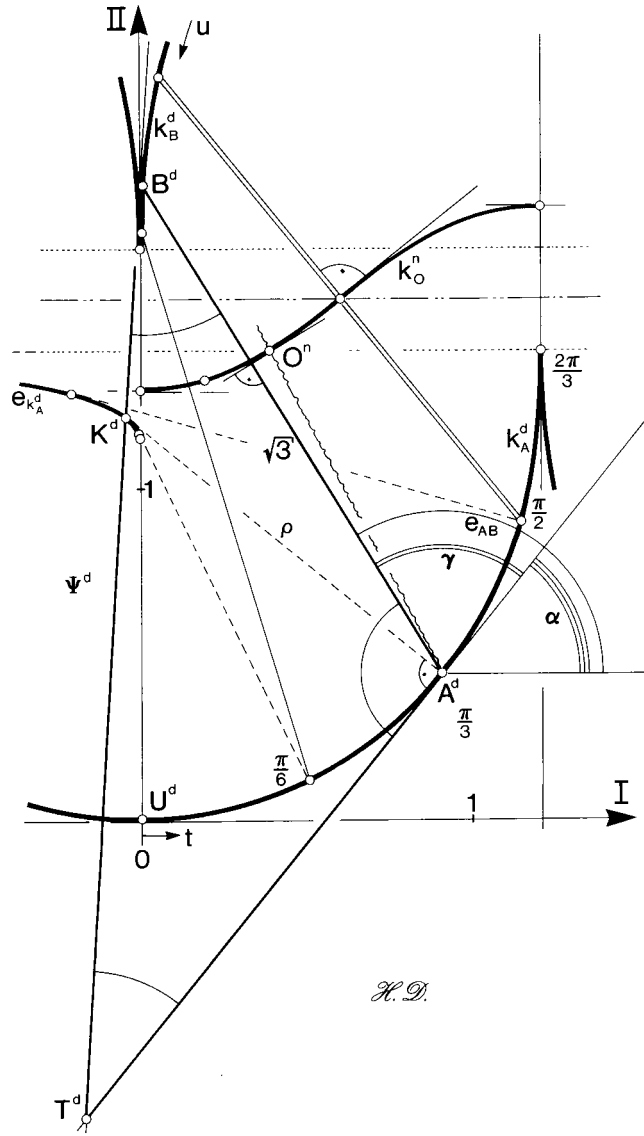


Figure 5: Detail of Fig. 4 with the image  $k_O^n$  of the center curve  $k_O$  under orthogonal projection into  $\tau$

In a similar way also the evolute  $e_{k_A^d}$  of  $k_A^d$  (see Fig. 4 or Fig. 5) can be computed. The parameter representation

$$\begin{aligned} I_K(t) &= I_A(t) - \rho \sin \alpha \\ II_K(t) &= II_A(t) + \rho \cos \alpha \end{aligned}$$

of  $e_{k_A^d}$  makes use of the curvature radius  $\rho$  according to (8). From (12) and (13) we obtain

$$\begin{aligned} \rho \sin \alpha &= \frac{(5 + 4 \cos t) \sqrt{6(1 - \cos t)}}{9 \sqrt{1 + 2 \cos t}} \\ \rho \cos \alpha &= \frac{2\sqrt{3}}{9} (1 + 2 \cos t) \end{aligned}$$



and finally as parametrization of the evolute  $e_{k_A^d}$  of  $k_A^d$

$$(19) \quad \begin{aligned} I_K(t) &= \frac{2\sqrt{3}}{9} \arccos \frac{\sqrt{2} \cos t}{\sqrt{1 + \cos t}} - \frac{\sqrt{2(1 - \cos t)}}{\sqrt{3(1 + 2 \cos t)}} \\ II_K(t) &= \frac{\sqrt{3}}{9} \left[ 6 + \ln \frac{2}{1 + \cos t} \right]. \end{aligned}$$

The evolute  $e_{k_A^d}$  obviously (see Fig. 4) does not pass through the cusps of  $k_A^d$ ; the curvature radius  $\rho$  tends to infinity. This reveals that these cuspidal points are not ordinary. For  $k_B^d$  the TAYLOR-series expansion of the parameter representation (18) at  $t = 0$  is

$$I_B(t) = \frac{1}{360} t^5 + O(t^7), \quad II_B(t) = \sqrt{3} + \frac{\sqrt{3}}{12} t^2 + O(t^4).$$

Therefore the singularities of  $k_A^d$  and  $k_B^d$  are of order 2 and class 3 (German: Rückkehrflachpunkte).

### 3 Motions Related to the Oloid

According to Fig. 3 we assume that the Oloid is rolling on the upper side of  $\tau$ . In the following we therefore choose for point  $B$  in (4) the negative  $z$ -coordinate. For the sake of brevity we substitute

$$(20) \quad s := \sin t \quad \text{and} \quad c := \cos t \quad \text{with} \quad -\frac{1}{2} < c \leq 1, \quad -1 \leq s \leq 1, \quad s^2 + c^2 = 1.$$

In order to describe the rolling of  $\Psi$  on  $\tau$  we introduce a moving frame of  $\Psi$  with origin  $A \in k_A$ . The first vector of this frame is the tangent vector  $\mathfrak{v}_A$  according to (15). The second vector  $\mathfrak{w}_A$  perpendicular to  $\mathfrak{v}_A$  is specified in the tangent plane  $\tau$ . We define

$$(21) \quad \mathfrak{w}_A := \frac{1}{\sin \gamma} \left( \frac{1}{\sqrt{3}} \overrightarrow{AB} - \mathfrak{v}_A \cos \gamma \right) = \frac{1}{\sqrt{2(1+c)}} \left( -s \sqrt{1+2c}, c \sqrt{1+2c}, -1 \right).$$

The vector

$$(22) \quad \mathfrak{n}_A := \mathfrak{v}_A \times \mathfrak{w}_A = \frac{1}{\sqrt{2(1+c)}} \left( -s, c, \sqrt{1+2c} \right)$$

perpendicular to  $\tau$  completes this cartesian frame.  $\mathfrak{n}_A$  is pointing to the interior of  $\Psi$ .

While the Oloid is rolling on the fixed plane  $\tau$ , the frame  $(A; \mathfrak{v}_A, \mathfrak{w}_A, \mathfrak{n}_A)$  shall be moving along  $\Psi$  in such a way, that  $A$  is the running point of contact between  $k_A$  and  $\tau$ . This implies that  $A \in k_A$  is always coincident with the corresponding point  $A^d \in k_A^d$ . Therefore the elements of the moving frame get the following coordinates with respect to the cartesian coordinate system  $(U^d; I, II, III)$  attached to  $\tau$ :

$$(23) \quad \begin{aligned} A &= (I_A(t), II_A(t), 0), & \mathfrak{v}_A &= (\cos \alpha, \sin \alpha, 0), \\ \mathfrak{w}_A &= (-\sin \alpha, \cos \alpha, 0), & \mathfrak{n}_A &= (0, 0, 1). \end{aligned}$$

Let  $(x, y, z)$  denote the coordinates of any point  $P$  attached to the Oloid. The required representation of the motion consists of a matrix equation which allows to compute the instantaneous coordinates  $(I, II, III)$  of point  $P$  with respect to the fixed plane  $\tau$ , in dependence

of the motion parameter  $t$ . In order to obtain this equation we firstly compute the coordinates  $(\xi, \eta, \zeta)$  of  $P$  with respect to the moving frame  $(A; \mathfrak{v}_A, \mathfrak{w}_A, \mathfrak{n}_A)$ . Though  $P$  is attached to  $\Psi$ , these coordinates are dependent on  $t$ . From (2), (15), (21) and (22) we get

$$(24) \quad \begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} s \\ -\frac{1}{2} - c \\ 0 \end{pmatrix} + \frac{1}{\sqrt{2(1+c)}} \begin{pmatrix} c\sqrt{2(1+c)} & -s\sqrt{1+2c} & -s \\ s\sqrt{2(1+c)} & c\sqrt{1+2c} & c \\ 0 & -1 & \sqrt{1+2c} \end{pmatrix} \begin{pmatrix} \xi \\ \eta \\ \zeta \end{pmatrix}.$$

Secondly, according to (23) the motion of the moving frame with respect to  $\tau$  (see Fig. 3) reads

$$\begin{pmatrix} I \\ II \\ III \end{pmatrix} = \begin{pmatrix} I_A(t) \\ II_A(t) \\ 0 \end{pmatrix} + \begin{pmatrix} \cos \alpha & -\sin \alpha & 0 \\ \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \xi \\ \eta \\ \zeta \end{pmatrix}.$$

Now we eliminate  $(\xi, \eta, \zeta)$  from these two matrix equations with orthogonal  $3 \times 3$ -matrices. After substituting (11), (12) and (13) we obtain by straight-forward calculation

**Theorem 4:** *Based on the cartesian coordinate systems  $(x, y, z)$  in the moving space and  $(I, II, III)$  in the fixed space, the rolling of the Oloid on the tangent plane  $\tau$  can be represented as*

$$\begin{pmatrix} I \\ II \\ III \end{pmatrix} = \frac{\sqrt{3}}{9} \begin{pmatrix} \frac{cs\sqrt{1+2c}}{2(1+c)\sqrt{2(1+c)}} + 2 \arccos \frac{c\sqrt{2}}{\sqrt{1+c}} \\ \frac{15+13c-c^2}{2(1+c)} + \ln \frac{2}{1+c} \\ \frac{3\sqrt{3}(2+c)}{2\sqrt{2(1+c)}} \end{pmatrix} + (a_{ij}) \begin{pmatrix} x \\ y \\ z \end{pmatrix}, \quad \text{where}$$

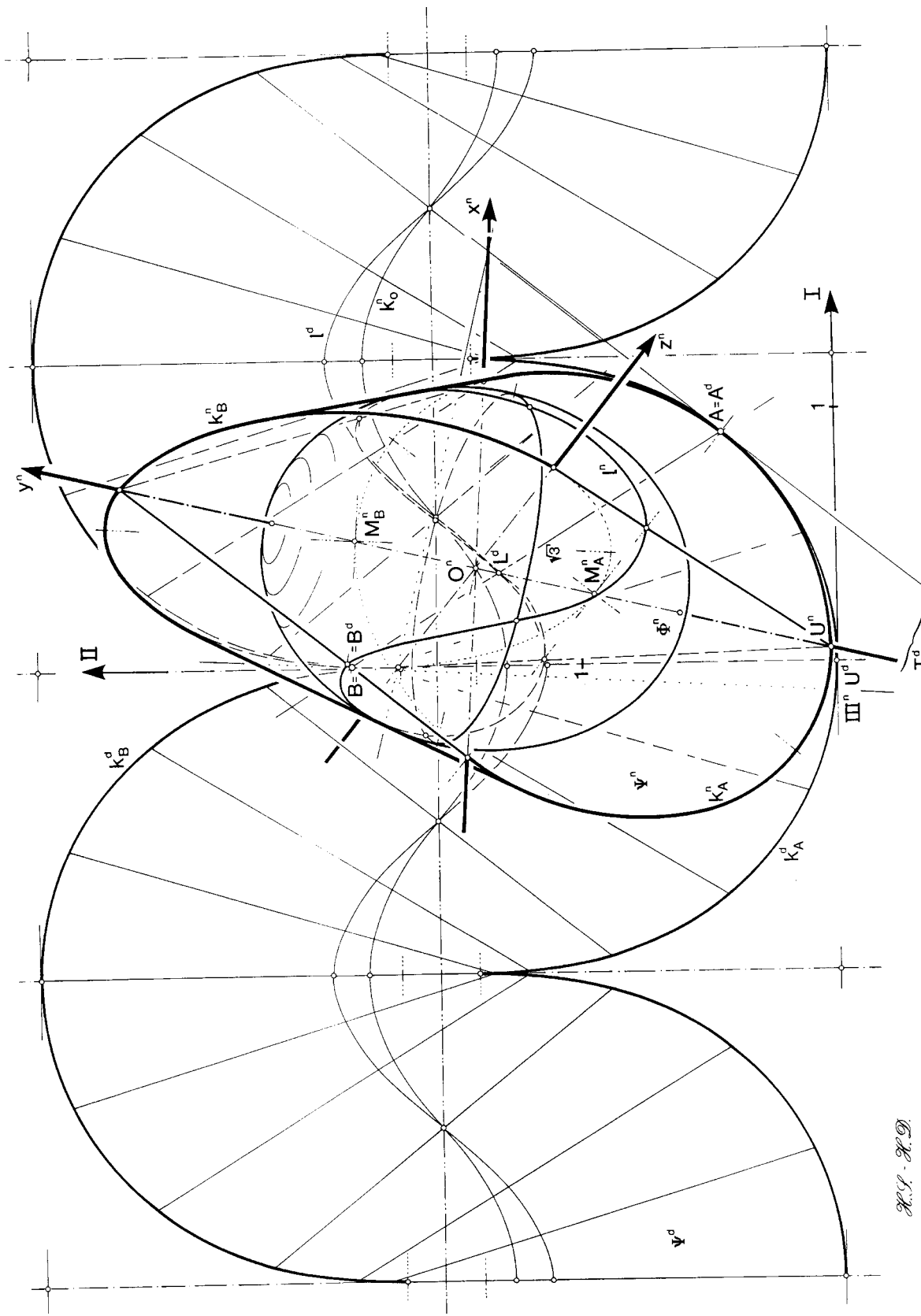
$$(a_{ij}) = \frac{\sqrt{3}}{9} \begin{pmatrix} \frac{(5+c)\sqrt{1+2c}}{\sqrt{2(1+c)}} & \frac{(2+c)s\sqrt{1+2c}}{(1+c)\sqrt{2(1+c)}} & \frac{(5+4c)s}{(1+c)\sqrt{2(1+c)}} \\ \frac{(c-1)s}{1+c} & \frac{5+5c-c^2}{1+c} & -\frac{(1+2c)\sqrt{1+2c}}{1+c} \\ -\frac{3s\sqrt{3}}{\sqrt{2(1+c)}} & \frac{3c\sqrt{3}}{\sqrt{2(1+c)}} & \frac{3\sqrt{3(1+2c)}}{\sqrt{2(1+c)}} \end{pmatrix}.$$

Here  $c$  and  $s$  stand for  $\cos t$  and  $\sin t$ , respectively, while the motion parameter  $t$  obeys (7).

The first vector on the right side of this matrix equation represents the path  $k_O$  of the Oloid's center  $O$  under this rolling motion. In particular, the third coordinate of this vector gives the oriented distance

$$(25) \quad r := \frac{2+c}{2\sqrt{2(1+c)}}$$

between  $O$  and the tangent plane for each  $t$ . Due to the introduced moving frame, this distance  $r$  equals the dot product  $\mathfrak{n}_A \cdot \overrightarrow{AO}$ . One can verify that for each  $t$  the velocity vector



*H. Stachel*

Figure 6: The Oloid and the inscribed ellipsoid  $\Phi$  are rolling on  $\tau$  while the curve  $l$  of contact between  $\Psi$  and  $\Phi$  traces  $l^d$

of the center curve  $k_O$  is perpendicular to the axis  $A^d B^d$  of the instantaneous rotation<sup>5</sup> (see orthogonal view  $k_O^n$  of  $k_O$  in Fig. 5 or Fig. 6).

The rolling of the Oloid is truly staggering. It is related to the Turbula motion (see [13] or [7]<sup>6</sup> and the references there) which is used for shaking liquids. It turns out that the Turbula motion is inverse to the motion of the moving frame in (24).

The circles  $k_A$  and  $k_B$  can also be seen as singular surfaces  $\widehat{k}_A, \widehat{k}_B$  of 2<sup>nd</sup> class. The coordinates  $(u_0 : u_1 : u_2 : u_3)$  of their tangent planes

$$u_0 + u_1 x + u_2 y + u_3 z = 0$$

match the “tangential equations”

$$\widehat{k}_A: 4u_0^2 - 4u_0 u_2 - 4u_1^2 - 3u_2^2 = 0, \quad \widehat{k}_B: 4u_0^2 + 4u_0 u_2 - 3u_2^2 - 4u_3^2 = 0.$$

Then due to a standard theorem of Projective Geometry the torse  $\Psi$  is not only tangent to  $k_A$  and  $k_B$  but to all surfaces of 2<sup>nd</sup> class included in the range which is spanned by  $\widehat{k}_A$  and  $\widehat{k}_B$ . Among these surfaces there is an ellipsoid  $\Phi$  of revolution<sup>7</sup> obeying the equation

$$(26) \quad \Phi: 6x^2 + 4y^2 + 6z^2 = 3 \quad \text{or} \quad \widehat{\Phi}: \frac{1}{2}(\widehat{k}_A + \widehat{k}_B) = 4u_0^2 - 2u_1^2 - 3u_2^2 - 2u_3^2 = 0$$

with focal points  $M_A, M_B$  and semi-axes  $\frac{\sqrt{3}}{2}$  and  $\frac{1}{\sqrt{2}}$  (cf. [13], p. 31). The curve  $l$  of contact between  $\Phi$  and the torse  $\Psi$  is located on cylinders which are the images of  $k_A$  and  $k_B$ , respectively, in the polarity with respect to  $\Phi$ . Therefore this curve has the representations

$$(27) \quad \begin{aligned} l: 3x^2 + \left(y - \frac{1}{2}\right)^2 &= 3z^2 + \left(y + \frac{1}{2}\right)^2 = 1 \quad \text{or} \\ x &= \frac{s}{2+c}, \quad y = -\frac{3c}{2(2+c)}, \quad z = \frac{\pm\sqrt{1+2c}}{2+c}. \end{aligned}$$

Together with the Oloid also the inscribed ellipsoid  $\Phi$  is rolling on  $\tau$ . In the fixed plane  $\tau$  the point of contact with the rolling ellipsoid traces a curve  $l^d$ . The parameter representation

$$(28) \quad l^d: I = \frac{2\sqrt{3}}{9} \arccos \frac{c\sqrt{2}}{\sqrt{1+c}}, \quad II = \frac{\sqrt{3}}{9} \left[ \ln \frac{2}{1+c} + \frac{3(5+c)}{2+c} \right], \quad III = 0$$

of this isometric image of  $l \subset \Psi$  is obtained by transforming the coordinates of  $l$  given in (27) (negative sign) under the matrix equation of Theorem 4.

Fig. 6 shows not only the fixed tangent plane  $\tau$  with the developed curves  $k_A^d, k_B^d$  and  $l^d$  in true shape. In this figure also an orthogonal view of the Oloid with the inscribed ellipsoid  $\Phi$  and the curve  $l$  of tangency is displayed.

<sup>5</sup>In general the instantaneous motion is a helical motion. However when a torse is rolling on a plane, the helical parameter must vanish (cf. [3], p. 161 or [6]).

<sup>6</sup>In this paper a very particular plane-symmetric six-bar loop is studied which is also displayed in [1], Figure 1. In each position of this loop and for each two opposite links  $\Sigma, \Sigma'$  there is a plane  $\tau$  of symmetry. It turns out that relatively to  $\Sigma$  these planes  $\tau$  are tangent to a torse of type  $\Psi$ . The Turbula motion is the motion of  $\Sigma$  relative to  $\tau$ , when in  $\tau$  the generator of the torse is kept fixed.

<sup>7</sup>In the cases treated in [5]  $k_A$  and  $k_B$  are ellipses, but  $\Phi$  is a sphere. This implies that the center  $O$  of gravity has a constant distance to  $\tau$  during the rolling motion.

## 4 Surface Area and Volume of the Oloid

As the development of a torse is locally an isometry, the computation of the area of  $\Psi$  can be carried out either in the 3-space or after the development into the plane  $\tau$ . We prefer the latter and use a formula given in [2], p. 118, eq. (5): The area swept out by the line segment  $AB$  under a planar motion for  $t_0 \leq t \leq t_1$  can be computed according to

$$(29) \quad S = \int_{t_0}^{t_1} \left\| \frac{1}{2}(\mathbf{v}_A + \mathbf{v}_B) \times \overrightarrow{AB} \right\| dt,$$

where  $\mathbf{v}_A, \mathbf{v}_B$  are the velocity vectors of the endpoints. For vectors in  $\mathbb{R}^2$  the norm in this formula can be cancelled which gives rise to an even oriented area.

In the coordinate system  $(I, II)$  of  $\tau$  we obtain due to (14) and (11)

$$\begin{aligned} \overrightarrow{AB} &= (\sqrt{3} \cos e_{AB}, \sqrt{3} \sin e_{AB}), \quad \mathbf{v}_A = \left( \frac{dI_A}{dt}, \frac{dII_A}{dt} \right), \\ \mathbf{v}_B &= \left( \frac{dI_A}{dt} - \sqrt{3} \sin e_{AB} \frac{de_{AB}}{dt}, \frac{dII}{dt} + \sqrt{3} \cos e_{AB} \frac{de_{AB}}{dt} \right) \end{aligned}$$

and according to (12) and (13)

$$\frac{dS}{dt} = \sqrt{3} \left( \frac{dI_A}{dt} \sin e_{AB} - \frac{dII_A}{dt} \cos e_{AB} \right) - \frac{3}{2} \frac{de_{AB}}{dt} = \sqrt{3} \sin \gamma - \frac{3}{2} \frac{de_{AB}}{dt}.$$

Eq. (16) and the derivation of (17) lead to

$$\frac{dS}{dt} = \frac{\sqrt{2(1+2\cos t)}}{\sqrt{1+\cos t}} - \frac{3\sqrt{2}\cos t}{2\sqrt{(1+\cos t)(1+2\cos t)}}$$

which finally results in

$$(30) \quad \frac{dS}{dt} = \frac{2 + \cos t}{\sqrt{2(1 + \cos t)(1 + 2 \cos t)}}.$$

After integration we obtain up to a constant  $k$

$$S(t) = \frac{1}{2} \left[ \arcsin \frac{1 - 4 \cos t}{3} - \arcsin \frac{1 + 5 \cos t}{3(1 + \cos t)} \right] + k$$

and for the complete torse  $\Psi$

$$(31) \quad S_\Psi = 8 \left[ S \left( \frac{\pi}{2} \right) - S(0) \right] = 4 \left[ S \left( \frac{2\pi}{3} \right) - S(0) \right] = 4\pi.$$

**Theorem 5:** *The surface area of the Oloid equals that of the unit sphere.*

The computation of the Oloid's volume starts from (30): Each surface element of  $\Psi$  is the base of a volume element forming a pyramid with apex  $O$ . Its altitude  $r$  has already been computed in (25) as it equals the distance between  $O$  and the corresponding tangent plane. Thus we obtain

$$(32) \quad dV = \frac{r}{3} dS = \frac{(2 + \cos t)^2}{12(1 + \cos t)\sqrt{1 + 2 \cos t}} dt.$$

A numerical integration gives

$$(33) \quad V_\Psi = 8 \left[ V \left( \frac{\pi}{2} \right) - V(0) \right] \approx 3.05241.$$

## Acknowledgements

The authors express their gratitude to Christine NOWAK (Klagenfurt) for her successful help in solving the integrals. Sincere thanks also for permanent contributions given by Jakob KOFLER (Klagenfurt). The authors are indebted to Gerhard HAINSCO (Wolfsberg) for fruitful discussions and to Sabine WILDBERGER (Klagenfurt) for manufacturing a model. Finally the authors thank Manfred HUSTY (Leoben) for useful comments and Gunter WEISS (Dresden) for pointing their attention to the singularities of  $k_A^d$  and  $k_B^d$ .

## References

- [1] J.E. BAKER: *The Single Screw Reciprocal to the General Plane-Symmetric Six-Screw Linkage*. JGG **1**, 5–12 (1997).
- [2] W. BLASCHKE, H.R. MÜLLER: *Ebene Kinematik*. Verlag von R. Oldenbourg, München 1956.
- [3] O. BOTTEMA, B. ROTH: *Theoretical Kinematics*. North-Holland Publ. Comp., Amsterdam 1979.
- [4] H. BRAUNER: *Lehrbuch der Konstruktiven Geometrie*. Springer-Verlag, Wien 1986.
- [5] C. ENGELHARDT, C. UCKE: *Zwei-Scheiben-Roller*. MNU, Math. Naturw. Unterr. **48/5**, 259–263 (1995).
- [6] M. HUSTY, A. KARGER, H. SACHS, W. STEINHILPER: *Kinematik und Robotik*. Springer, Berlin 1997.
- [7] S. KUNZE, H. STACHEL: *Über ein sechsgliedriges räumliches Getriebe*. Elem. Math. **29**, 25–32 (1974).
- [8] P. SCHATZ: Deutsches Reichspatent Nr. 589 452 (1933) in der allgemeinen Getriebe-klasse.
- [9] P. SCHATZ: *Rhythmusforschung und Technik*. Verlag Freies Geistesleben, Stuttgart 1975.
- [10] K. STRUBECKER: *Differentialgeometrie I*. 2. Aufl., Sammlung Göschen, Bd. 1113/1113a, Walter de Gruyter & Co, Berlin 1964.
- [11] K. STRUBECKER: *Differentialgeometrie II*. 2. Aufl., Sammlung Göschen, Bd. 1179/1179a, Walter de Gruyter & Co, Berlin 1969.
- [12] T.J. WILLMORE: *An Introduction to Differential Geometry*. Oxford University Press 1969.
- [13] W. WUNDERLICH: *Umwendung einer regelmäßigen sechsgliedrigen Würfelkette*. Proceedings IFToMM Symposium Mostar, May 1980, 23–33.

Received July 31, 1997; final form November 12, 1997