

Formulas used in ROBOT modules to calculate cross-sectional properties of the user-defined profiles (boxes, tubes, I-shapes)

### General remarks:

A complete set of formulas is given in the following tables. The tables are divided into four columns:

- |                |   |  |
|----------------|---|--|
| the 1st column | - | quantity symbol,   |
| the 2nd column | - | formula  |
| the 3rd column | - | comments (if necessary) about known incorrectness and planned modifications. The "FUNCTION" mark means planned replacement of the current pattern by the similar (precise) function of the characteristic diameters. |
| the 4th column | - | comments about formula origin (literature, where the formula may be found), and its precision with comparison to exact value.  |

All the definitions may describe the "thin" and "thick" profiles (in extrem the solid profiles may be defined). Hence, the separate formulas were used for both types of profiles (thin/thick). All the formulas were evaluated for the prismatic, elastic bars.

From all the quantities given below, only the  $A_x$  area is taken into account during the structure calculations (for Timoshenko's beam model, as well  $A_y$ ,  $A_z$ ). Others are used to estimate the stress values after the internal forces are known.

### Bibliography:

- |      |   |  |
|------|---|--|
| EG   | - | Elementary geometrical formulas  |
| EM   | - | Elementary formulas of the theory of elasticity  |
| EYR  | - | Handbook of steel constructions ("Guide pratique de charpente metallique" - R.Daussy - Eyrolles, 1987) |
| RCM  | - | Steel code "Regles de calculs des constructions en acier", Eyrolles, 1986                              |
| TIM  | - | "Theory of Elasticity" - Timoshenko, Goodier - McGraw-Hill, 1951                                       |
| WASH | - | "Variational Methods in Elasticity and Plasticity" - Washizu, Pergamon Press, 1975                     |

### Symbols and names:

- |       |   |  |
|-------|---|--|
| $A_x$ | - | cross-sectional area   |
| $A_y$ | - | reduced cross-sectional area to calculate "shear rigidity" (influence of the shearing force $F_y$ on beam deflections) |
| $A_z$ | - | reduced cross-sectional area to calculate "shear rigidity" (influence of the shearing force $F_z$ on beam deflections) |
| $W_x$ | - | torsional modulus ( $\tau_{max}=M_x/W_x$ )   |
| $W_y$ | - | reduced shear area ( $\tau_{ymax}=F_y/W_y$ )   |
| $W_z$ | - | reduced shear area ( $\tau_{zmax}=F_z/W_z$ )   |

## Definitions:

TUBE (pipe)

: R - external radius,  
r - internal radius

THICK profiles ( $r < 0.83R$ )			
Ax	$\pi * (R^2 - r^2)$		EG
Ay Az	$27/32 * Ax$		WASH - precise only for solid section. Unknown exact value for thick hollow sect.
Wx	$\pi * (R^4 - r^4) / 2R$		TIM
Wy Wz	$3/4 * Ax$	FUNCTION	RCM, TIM - precise only for solid section. Exact value in the range 0.75 - 0.5
THIN profiles ( $r > 0.83R$ )			
Ax	$\pi * (R^2 - r^2)$		EG
Ay Az	$0.5 * Ax$		WASH
Wx	$\pi * (R^4 - r^4) / 2R$		TIM
Wy Wz	$0.5 * Ax$		RCM, TIM - exact value for $r \rightarrow R$ (over 0.9R practically stable value of 0.5Ax)

BOX: h - web height  
ea - web thickness  
es - flange thickness  
b - flange width

THICK profiles ( $Ax > 1/3 b * (h + 2es)$ )			
Ax	$(h + 2es) * b - h * (b - 2ea)$		EG
Ay Az	$5/6 * Ax$		WASH - exact value for solid section. Unknown precise formula
Wx	$0.23 * Ax * \min(b, h)$		EYR - Weber's formula for solid section for others - unknown formula,
Wy Wz	$2/3 * Ax$	FUNCTION	RCM, TIM - exact value for solid section Precise value in the range 0.667 - 0.450
THIN profiles ( $Ax \leq 1/3 b * (h + 2es)$ )			
Ax	$(h + 2es) * b - h * (b - 2ea)$		EG
Ay	$2b * es$		Unknown origin
Az	$2(h + 2es) * ea$		Unknown origin
Wx	$2 * (h + es) * (b - ea) * \min(ea, es)$		Bredt's formula (EYR)
Wy	$5/6 * Ay$	FUNCTION	Exact value depends on proportion b/h (appx. 0.89 Ay)

Wz	$5/6 \cdot A_z$	FUNCTION	Exact value depends on proportion b/h (appx. 0.89 $A_y$ )
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RECT:     h - total height  
           ep - web and flange thickness  
           b - flange width

THICK profiles ( $A_x > 1/3 b \cdot h$ )			
Ax	$h \cdot b - (h - 2ep) \cdot (b - 2ep)$		EG
Ay Az	$5/6 \cdot A_x$		WASH - exact value for solid section Unknown precise formula
Wy Wz	$2/3 \cdot A_x$	FUNCTION	RCM, TIM - exact value for solid section precise formula in the range. 0.667 - 0.450
THIN profiles ( $A_x \leq 1/3 b \cdot h$ )			
Ax	$h \cdot b - h \cdot (b - 2ep)$		EG
Ay	$2b \cdot ep$		Unkown origin
Az	$2ep \cdot h$		Unkown origin
Wx	$2 \cdot (h - ep) \cdot (b - ep) \cdot ep$		Bredt's formula (EYR)
Wy	$5/6 \cdot A_y$	FUNCTION	Exact value depends on proportion b/h (appx. 0.89 $A_y$ )
Wz	$5/6 \cdot A_z$	FUNCTION	Exact value depends on proportion b/h (appx. 0.89 $A_z$ )

I-SECTION: h - web height  
           ea - web thickness  
           es - flange thickness  
           b - flange width

THICK profiles ( $A_x > 1/3 b \cdot (h + 2es)$ )			
Ax	$h \cdot ea + 2b \cdot es$		EG
Ay Az	$5/6 \cdot A_x$		WASH - exact value for solid section Unknown precise formula
Wx	$I_x / \max(ea, es)$		TIM - appx. formula
Wy Wz	$2/3 \cdot A_x$	FUNCTION	RCM, TIM - exact value for solid section precise formula in the range 0.667 - 0.450
THIN profiles ( $A_x \leq 1/3 b \cdot (h + 2es)$ )			
Ax	$h \cdot ea + 2b \cdot es$		EG
Ay	$2b \cdot es$		Flange area

Az	$h \cdot ea$		Web area
Wx	$I_x / \max(ea, es)$		TIM - appx. formula, for recatngles which ratio $b/h > 2.5$ (or $< 0.4$ ) - precise
Wy	$8I_z / (b^2 - ea^2)$		Manual calculations on the base of EM (as well RCM)
Wz	$8ea \cdot I_y / ((h+es) \cdot b^4 es + h^2 \cdot ea)$		Manual calculations on the base of EM (as well RCM)